

Optimal Under-frequency Load Shedding using Cuckoo Search with Levy Flight Algorithm for Frequency Stability Improvement

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Abstract— Frequency stability in a power system is very important as it determines the synchronous speed of electrical machines. Therefore it should remain within acceptable limits even when the system is disturbed. In order to ensure that frequency stability is achieved, load shedding is a countermeasure taken as a last resort. However, its consequences might result in huge technical and economic losses. Therefore, this control measure should be optimally and carefully carried out. This paper proposes Cuckoo search with Levy flights (CSwLF) based algorithm for solving the optimal load shedding problem. The amount of load shedding at each bus is determined by applying CSwLF to solve a nonlinear optimization problem formulated in the optimal power flow framework. The performance of the proposed CSwLF based method is tested on the operating conditions of IEEE 14-bus test system. The results shows that load shedding can be done discriminately in a single step to bring back a system from danger of frequency instability

Keywords— Metaheuristic algorithm, Frequency stability, under voltage load shedding, cuckoo search, Levy flights..

I. INTRODUCTION

Under-Frequency load shedding (UFLS) is defined as a coordinated act of controls, which results in the decrease of electrical loads in the power system. This act of possible corrective actions aims at forcing the perturbed system to a new equilibrium state (balancing the load and generation and thus maintaining system frequency within nominal range)

A power system will begin to deteriorate if there is an excess of load over available generation. The prime movers and their associated generators begin to slow down as they attempt to carry the excess load. Tie lines to other parts of the power system, attempt to supply the excess load. This combination of events can cause the tie lines to open from overload or the various parts of the systems to separate due to power swings and resulting instability. The result may be one or more electrically isolated islands in which load may exceed the available generation [1].

Further, the drop in frequency may endanger generation itself. While a hydro-electric plant is relatively unaffected by even a ten percent reduction in frequency, a thermal generating plant is quite sensitive to even a five percent reduction. Power output of a thermal plant depends to a great extent on its motor driven auxiliaries such as boiler feed water pumps, coal pulverizing and feeding equipment, and draft fans. As system frequency decreases, the power output to the auxiliaries begins to fall off rapidly which in turn further reduces the energy input to the turbine generator. The situation thus has a cascading effect with a loss of frequency leading to a loss of power which can cause the frequency to deteriorate further and the entire plant is soon in serious trouble. An additional major concern is the possible damage to the steam turbines due to prolonged operation at reduced frequency during this severe overload condition.

The objective of an under-frequency load shedding is to quickly recognize generation deficiency within any system and automatically shed a minimum amount of load, and at the same time provide a quick, smooth and safe transition of the system from emergency situation to a post-emergency condition such that a generation-load balance is achieved and nominal system frequency is restored

II. CUCKOO SEARCH ALGORITHM WITH LEVY FLIGHTS

A few metaheuristic optimization techniques have been proposed to solve load shedding problem. These includes Genetic Algorithm (GA) and Particle swarm optimisation (PSO) [2],[3]. A new metaheuristic search algorithm, called cuckoo search (CS), based on cuckoo bird's behavior has been developed by Yang and Deb [4]. However, the new stochastic search method, (CS), has not been applied to steady and dynamic state load shedding problem yet. This paper aims at establishing the applicability of this algorithm into load shedding.

The CS is derived from the bleeding behavior of some cuckoo species of laying their eggs in the nests of host birds.

Female cuckoos from some species of can imitate the patterns of the eggs of a few chosen host birds. This decreases the possibility of the eggs being abandoned and, therefore, increases their re-productivity [5]. If host birds discover the eggs are not their own, they will either throw them away or simply abandon their nests and build new ones, elsewhere. Parasitic cuckoo chooses a nest where the host bird just laid its own eggs and since the cuckoo eggs hatch slightly earlier than their host eggs, the first instinct action of the first cuckoo chick hatched is to evict the host eggs. This behaviour results in increasing the cuckoo chick's share of food provided by its host bird. In addition, Moreover, cuckoo chick can imitate the call of host chicks to gain access to more feeding opportunity [6],[7].

The Cuckoo Search models such breeding behavior. Yang and Deb discovered that the performance of the CS can be improved by using Lévy Flights instead of simple random walk. The variance of Levy flight increases exponentially as compared with random walk whose variance increases linearly. Therefore the convergence is faster with where step size is generated using Levy flights. Levy flights are more efficient in exploring unknown large scale search space [8], [9].

A solution is represented by an egg in the nest. A new solution is represented by a cuckoo egg. The CS endeavors to replace not-so-good solutions in the nests by the new and potentially better solutions represented by cuckoo's eggs. In the simplest form, each nest has one egg. The CS is based on three rules:

- Each cuckoo randomly lays one egg at a time in a nest;
- The best nest with high quality of eggs (solutions) will carry over to the next generations;
- The number of available host nests is fixed, and a host can discover an alien egg with probability $p_a \in [0,1]$. In this case, the host bird can either throw the egg away or abandon the nest to build a completely new nest in a new location [9]. The last assumption can be approximated by a fraction p_a of the n nests being replaced by new nests, having new random solutions. Based on the above-mentioned rules, the basic steps of the CS can be summarized as the pseudo code, as follows [9],[10].

Levy flights are random walk whose step length is drawn from the Levy distribution, often in terms of simple power-law formula.

$$L(u) = t^{-\lambda}, \quad 1 < \lambda \leq 3 \quad (1)$$

When generating new solutions $x_i(t+1)$ for the i^{th} cuckoo, the following Lévy flight is performed

$$x_i(t+1) = x_i(t) + \alpha \oplus Levy(\lambda) \quad (2)$$

where $\alpha > 0$ is the step size.

The product \oplus means entry-wise multiplications [9]. The generation of random numbers with Levy Flights consists of two steps: the choice of random direction which should be drawn from uniform distribution and generation of steps which obey Levy distribution. The generation of these steps is achieved using Mantegna algorithm for a symmetric Levy distribution. Here symmetric that the steps can be positive and negative. [10]. In Mantegna's algorithm, the step length s can be calculated by

$$s = \frac{u}{|v|^{1/\beta}} \quad (3)$$

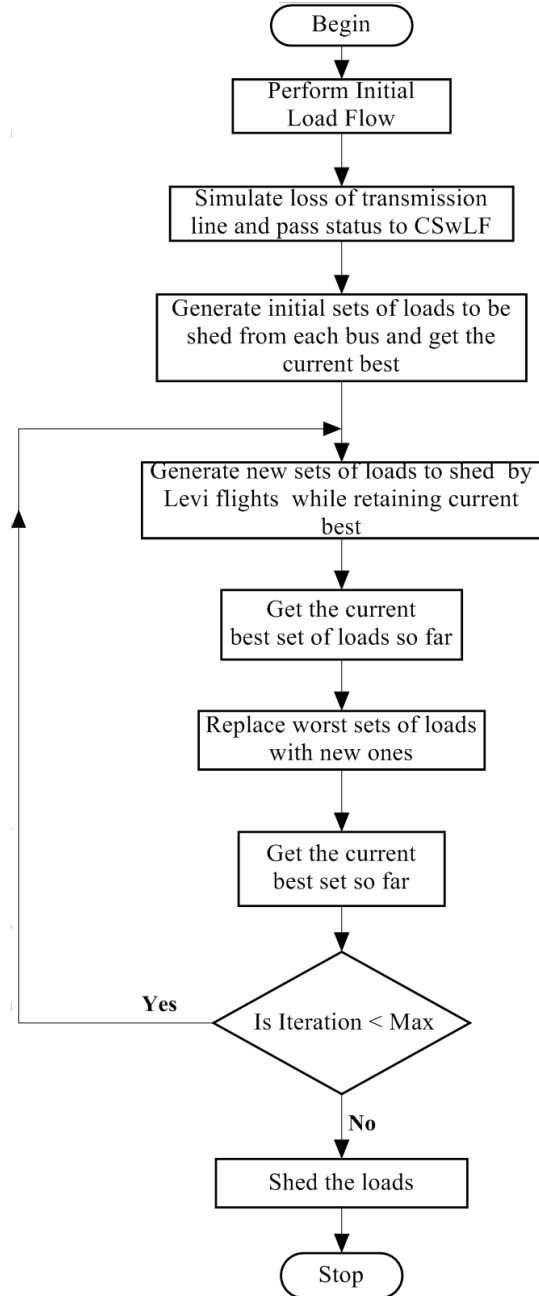
Where u and v are drawn from normal distribution. That is

$$u \sim N(0, \sigma_u^2), \quad v \sim N(0, \sigma_v^2)$$

Where

$$\sigma_u = \left\{ \frac{\Gamma(1 + \beta) \sin(\frac{\pi\beta}{2})}{\Gamma[(1 + \beta)/2] \beta 2^{(\beta-1)/2}} \right\}^{1/\beta}, \quad \sigma_v = 1 \quad (4)$$

In the application of the CS in load shedding, a nest has one egg. Therefore a nest or an egg represent a solution. One given solution comprises of the loads to be shed from each and every bus in the system. The number of available possible solutions was represented by the number of host nests available which was fixed. The initial solution was determined randomly with normal distribution. Its fitness was determined considering the equality and inequality constraints of the system. The best initial fitness is then carried over to the next set of solutions generated using CS with levy flight.



The fitness of the solutions is determined and the best solution is found. The worst solutions are discarded and replaced with new ones and the fitness of the new set is again determined.

The best solution is again found. The fitness of this best solution is checked to see whether it is within the acceptable tolerance. If it's not, the process starts over again

III. PROBLEM FORMULATION

During the UFLS, the following consideration need to be done:

- Facilities which are essential from a safety standpoint are not shed.
- The amount of load to be shed from the buses should correspond to the importance of that bus.
- The total amount of load shed should be the minimum possible, but sufficient to avoid the minimum allowable frequency being overcome.

This scenario is therefore formulated as an optimization problem with nonlinear constraints as follows: This scenario is therefore formulated as an optimization problem with nonlinear constraints as follows:

$$\text{Min} \sum_{i=1}^N [\alpha_i (P_{Di}^p - P_{Di}^0)^2] \quad (5)$$

This equation can be written as

$$\text{Min} \sum_{i=1}^N [\alpha_i \Delta P_{Di}^2] \quad (6)$$

Where

α_i are the importance factors for curtailed active power load of the i^{th} bus.

P_{Di}^0 = Active power demand in normal state

P_{Di}^p = Active power demand in contingency state

ΔP_{Di} is the curtailed active power of the i^{th} bus

Equality Constraints

$$P_{Gi}^p - P_{Di}^0 - \Delta P_{Di} - V_i^p \sum_{j=1}^N V_j^p Y_{ij} \cos(\delta_i - \delta_j - \theta_{ij}) = 0 \quad (7)$$

Where:

P_{Gi} and Q_{Gi} are active and reactive power generations at the i^{th} bus.

V_i and δ_i , are system bus voltages magnitudes and phase angles.

Y_{ij} and θ_{ij} are bus admittance matrix elements

Assuming that the increasing or decreasing of the active power generation of all generators was limited to 20% of their current generation, then:

$$0.8P_{Gi}^0 \leq P_{Gi}^p \leq 1.2P_{Gi}^0 \quad (8)$$

$$0.8Q_{Gi}^0 \leq Q_{Gi}^p \leq 1.2Q_{Gi}^0 \quad (9)$$

Assuming that all the buses have the same importance factor of 1, then:

$$0 \leq \Delta P_{Di} \leq P_{Di}^0 \quad (10)$$

IV. METHODOLOGY

The IEEE 14-bus system was selected for the study. The data for the system is readily available. The power flow analysis was first carried out using the Newton Raphson power flow technique to establish the loading levels of various transmission lines in the system. The main idea in this step is establish the heavily loaded line whose loss is likely to affect the performance of the entire system. This analysis was carried out using Power system Analysis Toolbox (PSAT). PSAT is a Matlab toolbox for static and dynamic analysis and control of electric power systems

A MATLAB code was developed to simulate loss of a transmission line through opening of circuit breaker associated to that line at time $t = 10s$, immediately capture this post contingency system status and pass it to the Cuckoo Search with Levy Flight algorithm to determine how much load need to be shed considering various constraints and finally simulate the load shedding.

After the algorithm determines the optimal load that need to be shed, the load shedding is simulated through opening of circuit breaker at time $t=16.75s$. This is the time the frequency drops to the minimum allowable value of 49.7 Hz or 0.994 p.u. The system status and parameters were again captured after the load had been shed to determine the effect of the load shedding.

V. RESULTS ANALYSIS

Table I shows the results obtained from power flow. Line 11 connected between Bus 1 and Bus 2 was the most heavily loaded line and its loss would be significant to the performance and equilibrium of the system. It's for this reason that this line was chosen for investigation.

Table I
Power Flow Results

From Bus	To Bus	Line	P Flow [p.u]	Q Flow [p.u]
Bus 2	Bus 5	1	0.4171	0.03219
Bus 6	Bus 12	2	0.08037	0.03119
Bus 12	Bus 13	3	0.01857	0.01353
Bus 6	Bus 13	4	0.18272	0.09743
Bus 6	Bus 11	5	0.0818	0.08439
Bus 11	Bus 10	6	0.04565	0.06399
Bus 9	Bus 10	7	0.04487	-0.00475
Bus 9	Bus 14	8	0.08719	0.00597
Bus 14	Bus 13	9	-0.06272	-0.04597
Bus 7	Bus 9	10	0.27203	0.1619
Bus 1	Bus 2	11	1.5712	-0.2046
Bus 3	Bus 2	12	-0.71124	0.01683
Bus 3	Bus 4	13	-0.23076	0.06689
Bus 1	Bus 5	14	0.7546	0.05482
Bus 5	Bus 4	15	0.6019	-0.09207
Bus 2	Bus 4	16	0.55939	0.01595
Bus 5	Bus 6	17	0.45689	0.10973
Bus 4	Bus 9	18	0.15504	0.02799
Bus 4	Bus 7	19	0.27203	-0.06506
Bus 8	Bus 7	20	0	0.25163

Figure 1 shows the frequencies of the most critical buses when line 11 was lost at $t=10s$. The figure shows that the frequencies in those buses fell below 49.7 Hz or 0.994 p.u. at time $t=16.7s$. This implies that the load shedding should occur not later than that time.

Table II shows the amount of load that need to be shed from every bus as determined by the Cuckoo Search with Levy Flight algorithm. Although all the buses were assumed to have equal importance, different amount of loads were to be shed from each bus. This is attributed to the fact that there were constraints conditions to be fulfilled for each bus. It is for this reason that no load was to be shed from buses 3 and 9.

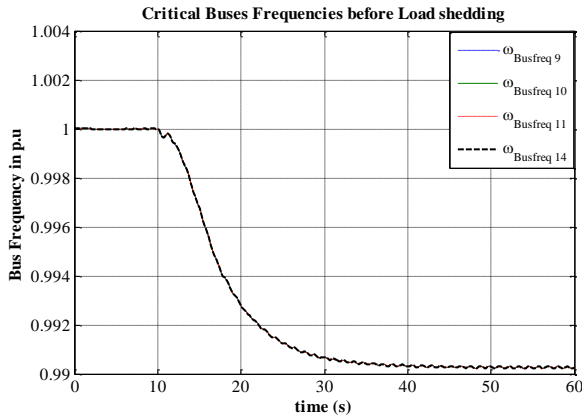


Figure 1 Critical Buses frequencies before load shedding

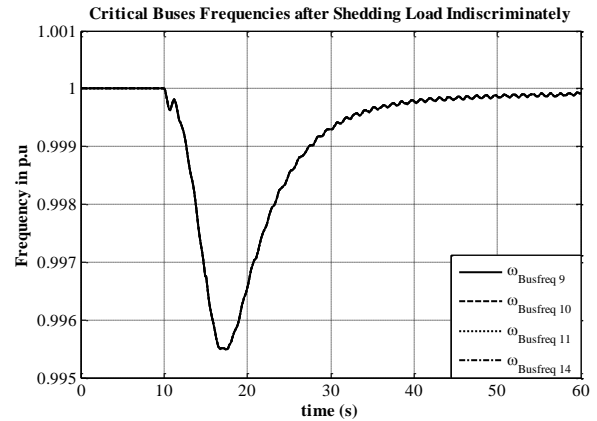


Figure 2 Critical Buses frequencies after load shedding without discrimination

Table II:
Amount of Load to be Shed from Each Bus

Bus No.	Bus Voltage	Load Demand		Load to Shed	
	(p.u)	MW	Mvar	MW (p.u)	Mvar (p.u)
1	1.06	0	0	0	0
2	1.05	0.217	0.127	0.0401	0
3	1.01	0.942	0.19	0	0
4	1.01	0.478	0.04	0.0019	0
5	1.02	0.076	0.016	0.0094	0
6	1.07	0.112	0.075	0.0293	0
7	1.05	0	0	0	0
8	1.09	0	0	0	0
9	1.03	0.295	0.166	0	0
10	1.03	0.09	0.058	0.045	0
11	1.05	0.035	0.018	0.0097	0
12	1.05	0.061	0.016	0.0259	0
13	1.05	0.135	0.058	0.0579	0
14	1.02	0.149	0.05	0.0636	0
TOTAL		2.59	0.814	0.2828	0

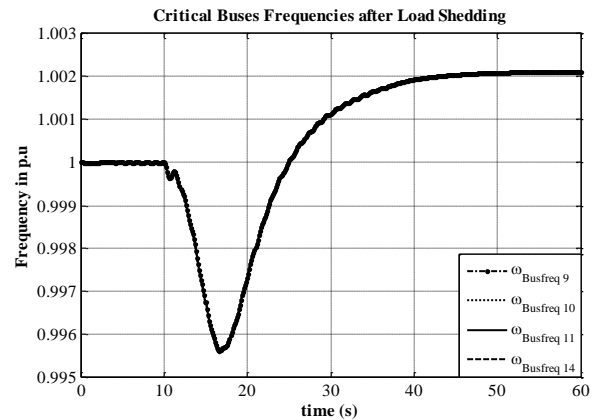


Figure 3 Critical Buses frequencies after load shedding with discrimination

Figure 2 shows that after an amount of 0.2828 p.u active load was shed at time $t=16.75s$, the frequency was restored back to acceptable limit. The frequency value did not go back to original value but to new value of 0.9999 p.u This is the new equilibrium state that the systems has taken after the contingency occurred. The load shedding was done in a single step as compared to traditional methods where load shedding is done in steps.

Figure 3 shows the frequencies of critical buses when the load shedding was done discriminately. Buses 5 and 12 were considered very important and hence no load was to be shed from them. It can be seen that even with shedding of load selectively, the frequency was restored back to acceptable limit. The frequency value did not go back to original value but to new value of 1.002 p.u

Table III
Active Load Shed from Buses with Equal Importance Factor of 0.5

Bus No.	Bus Voltage	Load Demand		Active Load Shed in p.u for a few runs						
	(p.u)	MW	Mvar	1	2	3	4	5	6	7
1	1.06	0	0	0	0	0	0	0	0	0
2	1.05	0.217	0.127	0.035	0.0593	0.0095	0.0259	0.0028	0	0.0035
3	1.01	0.942	0.19	0	0	0	0	0.0261	0.0095	0.0157
4	1.01	0.478	0.04	0.0036	0	0	0.0033	0.0118	0	0.0712
5	1.02	0.076	0.016	0.0241	0.0282	0.0092	0.038	0.0237	0.0373	0.038
6	1.07	0.112	0.075	0.0345	0.056	0.0182	0.056	0.0525	0.002	0.0318
7	1.05	0	0	0	0	0	0	0	0	0
8	1.09	0	0	0	0	0	0	0	0	0
9	1.03	0.295	0.166	0	0	0.0083	0.0038	0	0.0242	0.0179
10	1.03	0.09	0.058	0.045	0	0.0055	0.0446	0	0.0449	0.0007
11	1.05	0.035	0.018	0.0163	0	0.0119	0.0171	0.0175	0.0014	0.0057
12	1.05	0.061	0.016	0.0185	0.0209	0.0036	0.0131	0.0251	0.0072	0.0304
13	1.05	0.135	0.058	0	0.0128	0.0325	0.0203	0.0212	0.0559	0
	1.02	0.149	0.05	0	0	0.0038	0.0403	0.0319	0	0.0614
TOTAL		2.59	0.814	0.177	0.1772	0.1025	0.2624	0.2126	0.1824	0.2763

Table IV
Active Load Shed from Buses with Unequal Importance Factor

Bus No.	Bus Voltage	Load Demand		Active Load Shed in p.u for a few runs						
	(p.u)	MW	Mvar	1	2	3	4	5	6	7
1	1.06	0	0	0	0	0	0	0	0	0
2	1.05	0.217	0.127	0.0537	0.0439	0	0.0117	0.0039	0.0365	0
3	1.01	0.942	0.19	0.0283	0	0.027	0	0.0171	0	0.0025
4	1.01	0.478	0.04	0	0.0313	0.0312	0	0.004	0.0076	0.0021
5	1.02	0.076	0.016	0	0	0	0	0	0	0
6	1.07	0.112	0.075	0	0.0479	0	0.056	0.0015	0.0407	0.0277
7	1.05	0	0	0	0	0	0	0	0	0
8	1.09	0	0	0	0	0	0	0	0	0
9	1.03	0.295	0.166	0	0.0167	0	0.0102	0.0065	0	0
10	1.03	0.09	0.058	0.0216	0.0384	0	0	0.045	0.0268	0.0036
11	1.05	0.035	0.018	0.0096	0.011	0.0056	0.0147	0	0.0055	0.0163
12	1.05	0.061	0.016	0	0	0	0	0	0	0
13	1.05	0.135	0.058	0.003	0	0.0015	0.0121	0	0	0
14	1.02	0.149	0.05	0	0	0.0085	0.067	0.0076	0.0035	0
TOTAL		2.59	0.814	0.1162	0.1892	0.0738	0.1717	0.0856	0.1206	0.0522

Table III shows the amount of load shed from the buses for several runs with all buses treated equally i.e with equal importance factor of 0.5. No load was shed from buses 1, 7 and 8 since no load is connected to those buses.

Table IV shows the amount of load shed from the buses for several runs with the buses treated differently. The importance factor ranges from 0 to 1 with 1 being the least important and 0 being the most important. Therefore buses 5 and 12 were assigned importance factor of 0. With Buses 5 and Buses 12 being treated as very important, no load was shed from these buses. This means that the load shedding was done discriminately depending on the importance factor of the bus.

VI. CONCLUSION

The above results shows that load shedding using Cuckoo search with Levy flights can be done in a single step to bring back a system from danger of frequency instability. It also shows that it is possible to spare very important facilities from disconnection without compromising on system stability

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